

# HelixTrack: Event-Based Tracking and RPM Estimation of Propeller-like Objects

## Supplementary Material

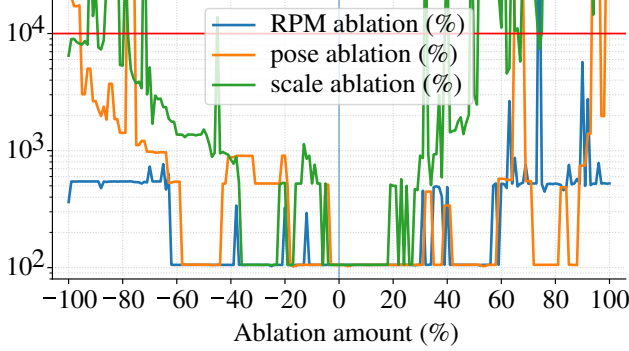


Figure S1. Robustness to initialization errors. We perturb the initial tracker position, in-plane scale, and initial RPM by  $\pm\{1, 2, \dots, 100\}\%$  around the nominal initialization and run HelixTrack end-to-end. For position, we average shifts “toward” and “away from” the nearest distractor (propeller). The plot reports shaft-RPM Mean Absolute Error (MAE) across propellers with  $\text{MAE} \leq 300$  (lower is better); red line marks 10,000 RPM.

### S1. Robustness to initialization errors

In this section, we present the figure showing robustness of HelixTrack to initialization errors Fig. S1.

### S2. Full Gauss-Newton System with Jacobians

In this section, we describe the full Gauss-Newton System with Jacobians of the terms mentioned in Sec. 3.

**Jacobians for all residuals.** Let  $\sigma(x) = \frac{1}{1+e^{-x}}$  and adopt  $\frac{d}{dx} \text{wrap}_\pi(x) = 1$  a.e. For polarity,

$$\delta_i = \text{wrap}_\pi(\varepsilon_i^\phi - d_{\text{pol}}), \quad \varepsilon_i^{\text{pol}} = c_{\text{pol}} \sin(\frac{1}{2}\delta_i),$$

$$\mathbf{J}_i^{\text{pol}} = c_{\text{pol}} \cdot \frac{1}{2} \cos(\frac{1}{2}\delta_i) \mathbf{J}_i^\phi.$$

For soft band barriers,

$$\varepsilon_i^{\text{in}} = c_b \text{softplus}_\tau(r_{\text{in}} - r_i), \quad \varepsilon_i^{\text{out}} = c_b \text{softplus}_\tau(r_i - r_{\text{out}}),$$

$$\mathbf{J}_i^{\text{in}} = -c_b \sigma\left(\frac{r_{\text{in}} - r_i}{\tau}\right) \mathbf{J}_i^r, \quad \mathbf{J}_i^{\text{out}} = c_b \sigma\left(\frac{r_i - r_{\text{out}}}{\tau}\right) \mathbf{J}_i^r.$$

**Balanced Tip Occupancy (BTO).** Define soft occupancies with temperature  $\tau_{\text{occ}}$ ,

$$m_i^{\text{in}} = \sigma\left(\frac{r_{\text{in}} - r_i}{\tau_{\text{occ}}}\right), \quad m_i^{\text{out}} = \sigma\left(\frac{r_i - r_{\text{out}}}{\tau_{\text{occ}}}\right),$$

$$p_{\text{in}} = \frac{1}{|\mathcal{B}|} \sum_i m_i^{\text{in}}, \quad p_{\text{out}} = \frac{1}{|\mathcal{B}|} \sum_i m_i^{\text{out}}.$$

Then

$$\frac{\partial p_{\text{in}}}{\partial \mathbf{q}} = \frac{1}{|\mathcal{B}|} \sum_i \left[ -\frac{1}{\tau_{\text{occ}}} m_i^{\text{in}} (1 - m_i^{\text{in}}) \mathbf{J}_i^r \right],$$

$$\frac{\partial p_{\text{out}}}{\partial \mathbf{q}} = \frac{1}{|\mathcal{B}|} \sum_i \left[ \frac{1}{\tau_{\text{occ}}} m_i^{\text{out}} (1 - m_i^{\text{out}}) \mathbf{J}_i^r \right].$$

Let

$$\phi(s) = \text{softplus}_\tau(s), \quad \phi'(s) = \sigma(s/\tau),$$

$$\phi''(s) = \sigma(s/\tau)(1 - \sigma(s/\tau))/\tau$$

and

$$s_{\text{in}}^{\text{lo}} = \underline{p}_{\text{in}} - p_{\text{in}}, \quad s_{\text{in}}^{\text{hi}} = p_{\text{in}} - \overline{p}_{\text{in}},$$

$$s_{\text{out}}^{\text{lo}} = \underline{p}_{\text{out}} - p_{\text{out}}, \quad s_{\text{out}}^{\text{hi}} = p_{\text{out}} - \overline{p}_{\text{out}}.$$

Hence

$$\mathbf{J}_{s_{\text{in}}^{\text{lo}}} = -\frac{\partial p_{\text{in}}}{\partial \mathbf{q}}, \quad \mathbf{J}_{s_{\text{in}}^{\text{hi}}} = \frac{\partial p_{\text{in}}}{\partial \mathbf{q}}, \quad \mathbf{J}_{s_{\text{out}}^{\text{lo}}} = -\frac{\partial p_{\text{out}}}{\partial \mathbf{q}}, \quad \mathbf{J}_{s_{\text{out}}^{\text{hi}}} = \frac{\partial p_{\text{out}}}{\partial \mathbf{q}}.$$

**Complete GN system.** With frozen gates  $g_i^\phi = \lambda_\phi w_i^\phi$  and  $g_i^r = \lambda_r w_i^r$ ,

$$\mathbf{H}_{\text{GN}} = \sum_i g_i^\phi (\mathbf{J}_i^\phi)^\top \mathbf{J}_i^\phi + \sum_i g_i^r (\mathbf{J}_i^r)^\top \mathbf{J}_i^r \quad (\text{S1})$$

$$+ \lambda_{\text{pol}} \sum_i (\mathbf{J}_i^{\text{pol}})^\top \mathbf{J}_i^{\text{pol}} \quad (\text{S2})$$

$$+ \lambda_{\text{band}} \sum_i \left[ (\mathbf{J}_i^{\text{in}})^\top \mathbf{J}_i^{\text{in}} + (\mathbf{J}_i^{\text{out}})^\top \mathbf{J}_i^{\text{out}} \right] \quad (\text{S3})$$

$$+ \lambda_{\text{BTO}} \sum_{q \in \{\text{in}, \text{out}\}} \left[ \phi''(s_q^{\text{lo}}) (\mathbf{J}_{s_q^{\text{lo}}})^\top \mathbf{J}_{s_q^{\text{lo}}} \right] \quad (\text{S4})$$

$$+ \phi''(s_q^{\text{hi}}) (\mathbf{J}_{s_q^{\text{hi}}})^\top \mathbf{J}_{s_q^{\text{hi}}} \quad (\text{S5})$$

$$+ \mathbf{H}_{\text{reg}}, \quad (\text{S6})$$

$$\mathbf{g} = \sum_i g_i^\phi \varepsilon_i^\phi (\mathbf{J}_i^\phi)^\top + \sum_i g_i^r \varepsilon_i^r (\mathbf{J}_i^r)^\top \quad (\text{S7})$$

$$+ \lambda_{\text{pol}} \sum_i \varepsilon_i^{\text{pol}} (\mathbf{J}_i^{\text{pol}})^\top \quad (\text{S8})$$

$$+ \lambda_{\text{band}} \sum_i \left[ \varepsilon_i^{\text{in}} (\mathbf{J}_i^{\text{in}})^\top + \varepsilon_i^{\text{out}} (\mathbf{J}_i^{\text{out}})^\top \right] \quad (\text{S9})$$

$$+ \lambda_{\text{BTO}} \sum_{q \in \{\text{in}, \text{out}\}} \left[ \phi'(s_q^{\text{lo}}) (\mathbf{J}_{s_q^{\text{lo}}})^\top + \phi'(s_q^{\text{hi}}) (\mathbf{J}_{s_q^{\text{hi}}})^\top \right] \quad (\text{S10})$$

$$+ \mathbf{g}_{\text{reg}}. \quad (\text{S11})$$

### S3. Dataset Details

This section gives a detailed overview of Timestamped Quadcopter with Egomotion dataset.

The average number of ground-truth timestamps is 4 770, maximum 5 116, minimum 4 906, and median is 4 876.

The average number of processed events is  $1.7 \times 10^9$ , maximum  $3.1 \times 10^9$ , minimum  $1.0 \times 10^9$ , and median is  $1.6 \times 10^9$ .

The average event rate is  $60,4 \times 10^6$  (events / second).

In Fig. S2, the aggregated events of the first 10 ms of five 1-second intervals are displayed for all recordings taken at a camera-to-quadcopter distance of 2 m. The intensity of egomotion begins at the top with  $M_{\text{ego}} = 1$  and progresses to the last row with  $M_{\text{ego}} = 7$ . Fig. S3 is structured in the same way and presents recordings for a camera-to-quadcopter distance of 4 m.

### S4. AEB-Tracker Parameters Grid Search

As described in Sec. 4.3.1, we first tuned the hyperparameters of the tracker qualitatively. Once a well-performing set of parameters was found on the first 10 milliseconds of the recording, we run the grid search described below.

We performed a comprehensive grid search over four AEB-tracker hyperparameters, 72 combinations in total, evaluated across all recordings and channels. The parameters are as follows.

1.  $rb$  (ring\_buffer\_len): Length of the per-target event/state ring buffers. Larger values smooth estimates more but add inertia,
2.  $\Delta t$ : Integration timestep (seconds) used in the state transition  $F$  for  $(x, y, \theta)$ ; in particular  $\dot{\theta} \leftarrow \dot{\theta} + q \, dt$ ,
3.  $q_{xy}$ : Sets both velocity process-noise intensities  $q_{v_x}$  and  $q_{v_y}$  [ $\text{px}^2/\text{s}^3$ ]. Larger values allow faster changes in velocity (more agility) at the cost of more noise/jitter.
4.  $q_q$ : Sets the spin-rate process-noise intensity  $q_q$  [ $\text{rad}^2/\text{s}^3$ ]. Larger values let the angular velocity  $q$  vary more between updates.

We select the setting that minimizes mean absolute error (MAE). We also report std/median and mean absolute relative error (MArE).

The best configuration observed in Table S4 is  $rb = 22$ ,  $\Delta t = 2.5$ ,  $q_{xy} = 5.0$ ,  $q_q = 0.5$ , achieving MArE 502.976 and MAE of 38763.807 (aggregated over all recordings and channels).

### S5. HelixTrack Parameter and Grid Search

We set the parameters of HelixTrack with a combination of element-wise search and grid search. The complete set of parameters we searched for and their final values are:  $q_{\text{jerk}} = 400$ ,  $\lambda_\phi = 1.0$ ,  $\lambda_r = 1.0$ ,  $\lambda_{\text{pol}} = 0.25$ ,  $\lambda_{\text{band}} = 5.0$ ,  $\lambda_{\text{BTO}} = 1.0$ ,  $r_{\text{in}} = 0.2$ ,  $r_{\text{out}} = 1.5$ ,  $\gamma_{\text{tx}} = \gamma_{\text{ty}} = 6.0$ ,  $\gamma_{\text{persp}} = 1.0$ . For the complete set of all parameters, not just

$r_{\text{in}}$	$r_{\text{out}}$	MAE (RPM) ↓	median
0.0	1.4	25897.838 ± 64560.838	6837.504
0.0	1.5	31173.431 ± 89359.956	6623.163
0.0	1.6	21958.240 ± 62330.271	7017.397
0.0	1.7	33919.799 ± 133795.000	7763.656
0.0	1.8	17984.723 ± 43510.488	6545.428
0.0	1.9	15783.097 ± 43241.885	7078.281
0.1	1.4	4356.810 ± 3985.889	4434.631
0.1	1.5	4814.578 ± 5064.586	4995.041
0.1	1.6	4775.841 ± 3918.283	6323.458
0.1	1.7	4951.189 ± 4428.663	5219.091
0.1	1.8	4687.726 ± 4220.879	5265.247
0.1	1.9	10199.062 ± 39763.741	5339.970
0.2	1.4	10659.736 ± 44302.860	5516.170
<b>0.2</b>	<b>1.5</b>	<b>4052.139 ± 3779.222</b>	<b>5200.247</b>
0.2	1.6	4626.934 ± 3815.512	6050.976
0.2	1.7	4574.203 ± 4136.607	5391.578
0.2	1.8	4691.997 ± 4598.824	5790.502
0.2	1.9	4500.675 ± 3892.523	5436.960
0.3	1.4	6470.363 ± 12126.974	6095.369
0.3	1.5	4401.135 ± 3951.049	5629.956
0.3	1.6	43303.116 ± 274072.299	5758.449
0.3	1.7	4846.586 ± 5777.108	5273.668
0.3	1.8	5826.368 ± 8064.029	5181.593
0.3	1.9	29329.222 ± 179744.825	5588.616

Table S1. Grid search over  $r_{\text{in}}$  and  $r_{\text{out}}$  with  $q_{\text{jerk}}=400$ ,  $\lambda_\phi=1.0$ ,  $\lambda_r=1.0$ ,  $\lambda_{\text{pol}}=0.25$ ,  $\lambda_{\text{band}}=5.0$ ,  $\lambda_{\text{BTO}}=1.0$ ,  $\gamma_x=\gamma_y=6.0$ ,  $\gamma_{\text{persp}}=1.0$ . The best setting (lowest MAE mean) is highlighted in bold. See Sec. S5

the ones we searched for, see the attached configuration file and codes.

The grid search was performed over  $r_{\text{in}}$  and  $r_{\text{out}}$  parameters, results are in Table S1.

The element-wise search was performed with the following set of parameters:

- $q_{\text{jerk}}$  (7): 50, 100, 200, 300, 400, 500, 600
- $\lambda_\phi$  (2): 0, 1
- $\lambda_r$  (2): 0, 1
- $\lambda_{\text{pol}}$  (6): 0, 0.25, 0.5, 1, 2, 10
- $\lambda_{\text{band}}$  (5): 0, 1, 5, 10, 20
- $\lambda_{\text{tip}}$  (5): 0, 0.5, 1, 2, 10
- $\gamma_x=\gamma_y$  (7): 1, 2, 3, 4, 5, 6, 7
- $\gamma_{\text{persp}}$  (5): 0.01, 0.1, 1, 2, 3

In total, **275** unique experiment configurations were examined, not including the grid search for  $r_{\text{in}}$  and  $r_{\text{out}}$ .

### S6. Benchmark Complete Results

Across all cells of the Table S3, HelixTrack is consistently the most accurate. It achieves the lowest error in



Figure S2. Aggregated events from all sequences in the Timestamped Quadcopter with Egomotion dataset with camera-to-quadcopter distance of 2 m, from the smallest (top row,  $M_{\text{ego}}=1$ ), to the largest (bottom row,  $M_{\text{ego}}=7$ ) egomotion intensity. Events from the first 10 ms of five 1-second intervals are shown. Positive events displayed in black, negative in gray.

43/52 (MArE), 46/52 (MAE), and 45/52 (RMSE) cases, while AEB-Tracker wins 8/6/5 and DeepEv 1/0/2, respectively. When we compute medians to mitigate heavy-tailed failures, HelixTrack reduces error dramatically relative to AEB-Tracker — MArE: 400.05  $\rightarrow$  58.95 (-85.3%), MAE: 29,859.50  $\rightarrow$  5,200.3 (-82.6%), RMSE: 51,662.7  $\rightarrow$  6,332.25 (-87.7%). DeepEv’s medians for MAE/RMSE (14,459.0 / 19,504.4) are below the medians of AEB-Tracker, but its means are much higher due to frequent catastrophic failures.

**Effect of distance  $d$ .** Performance improves with increased camera–scene distance for HelixTrack. At  $d = 2\text{m}$  vs.  $4\text{m}$ , HelixTrack’s medians drop from 63.65  $\rightarrow$  29.65 (MArE), 5,233.10  $\rightarrow$  2,697.55 (MAE), and 6,461.30  $\rightarrow$  3,358.60 (RMSE). Compared to AEB-Tracker, the improvement widens at longer distance:  $d = 2\text{m}$ : -84.1% / 82.5% / 87.5%

(MArE/MAE/RMSE);  $d = 4\text{m}$ : -94.9% / 94.0% / 95.5%. A plausible explanation is that the propeller occupies a smaller angular extent and generates fewer disruptive events at larger  $d$ , which HelixTrack exploits more effectively than the baselines.

**Effect of ego-motion magnitude  $M_{\text{ego}}$ .** As motion increases, all methods degrade, but HelixTrack degrades more gracefully. For MAE (medians), HelixTrack stays low for  $M_{\text{ego}} = 1 - 3$ , and rises for  $M_{\text{ego}} = 4 - 7$  — still well below the results of AEB-Tracker. AEB-Tracker shows a pronounced failure at moderate-to-high motion (also reflected in RMSE), while DeepEv exhibits a non-monotonic pattern with moderate medians at certain bins but very heavy tails overall.

**Sensitivity to propeller position.** The position of a propeller with respect to other propellers / distractors, mat-



Figure S3. Aggregated events from all sequences in the Timestamped Quadcopter with Egomotion dataset with camera-to-quadcopter distance of 4 m, from the smallest (top row,  $M_{\text{ego}}=1$ ), to the largest (bottom row,  $M_{\text{ego}}=7$ ) egomotion intensity. Events from the first 10 ms of five 1-second intervals are shown. Positive events displayed in black, negative in gray.

ters., HelixTrack’s easiest configuration is front-left. The most challenging is rear-right, followed by front-right and rear-left. Despite this, HelixTrack still secures the majority of wins in every placement: for example, in front-left it wins 13/13 cells for each metric, and even in rear-right it wins 12/13 (MAE/RMSE) and 11/13 (MArE).

AEB-Tracker collects isolated wins (*e.g.*, low motion with favorable geometry), and DeepEv takes two RMSE cells in specific configurations. However, these wins are not robust: the corresponding 95th percentiles and maxima reveal frequent large errors and outright failures, especially for DeepEv. In contrast, HelixTrack shows low variance in most of the grid.

## S7. Loss ablation

The results of the loss term ablation in Table S2 show that removing either the phase-geometry coupling ( $\lambda_{\phi} = 0$ ) or the radial centering term ( $\lambda_r = 0$ ) leads to failure or order-of-magnitude error increases. For example, at 2 m,  $M_{\text{ego}} = 2$ , MAE jumps from  $90.1 \pm 16.9$  (full loss) to

$9327.1 \pm 175.7$  when  $\lambda_r = 0$ ; at 4 m,  $M_{\text{ego}} = 3$  it rises from  $3449.3 \pm 3961.3$  to  $9775.1 \pm 129.5$  when  $\lambda_r = 0$ . Tying the Gauss-Newton pose update to phase residuals  $r_{\phi}$  and keeping events centered on the blade ring via  $r_r$  are important for stabilizing geometry and phase jointly (Sec. 3.5, Eq. 4).

Disabling the soft band-edge barriers ( $\lambda_{\text{band}} = 0$ ) frequently causes failures in the harder settings (average column reports failure; *e.g.*, 2 m,  $M_{\text{ego}} = 4$  and 2 m,  $M_{\text{ego}} = 7$  both fail), indicating that the annulus constraints are necessary to keep the optimization from leaking inside/outside the informative blade band when background motion and perspective effects are large.

Dropping the polarity term ( $\lambda_{\text{pol}} = 0$ ) degrades the overall average from  $4052.1 \pm 2135.0$  to  $7070.4 \pm 3146.3$  and can sharply increase error in challenging cases (*e.g.*, 4 m,  $M_{\text{ego}} = 4$ :  $2152.1 \pm 4126.9$  to  $8055.4 \pm 1451.6$ ), suggesting that softly aligning polarity clusters with the expected blade edge improves robustness.

Removing BTO ( $\lambda_{\text{BTO}} = 0$ ) changes the overall average

$d$	$M_{\text{ego}}$	all	$\lambda_\phi = 0$	$\lambda_r = 0$	$\lambda_{\text{pol}} = 0$	$\lambda_{\text{band}} = 0$	$\lambda_{\text{BTO}} = 0$
2 m	1	<b>92.8 ± 18.4</b>	98.8 ± 21.5	<i>F</i>	5701.9 ± 3786.9	<b>92.8 ± 18.4</b>	92.8 ± 18.4
2 m	2	90.1 ± 16.9	2347.5 ± 2766.6	9327.1 ± 175.7	2103.3 ± 4024.6	<b>89.7 ± 16.6</b>	90.1 ± 16.9
2 m	3	680.2 ± 974.9	3883.1 ± 7372.4	8430.9 ± 1589.7	7438.6 ± 1700.5	1319.7 ± 1522.6	<b>612.5 ± 841.1</b>
2 m	4	7212.5 ± 332.2	7807.8 ± 3357.2	8720.0 ± 1068.0	7427.7 ± 950.7	<i>F</i>	<b>6821.1 ± 475.0</b>
2 m	5	7488.4 ± 2162.5	<b>6718.4 ± 2246.1</b>	<i>F</i>	7142.7 ± 1866.7	7452.8 ± 1056.6	8434.2 ± 974.4
2 m	6	7981.4 ± 1705.1	8902.2 ± 307.7	8210.8 ± 2099.4	8182.7 ± 1695.0	7997.8 ± 1939.9	<b>7868.9 ± 899.4</b>
2 m	7	<b>6497.4 ± 1534.1</b>	<i>F</i>	9194.3 ± 240.5	7873.5 ± 1519.3	<i>F</i>	8032.8 ± 573.4
4 m	1	<b>1721.3 ± 3263.3</b>	2176.4 ± 4171.0	9056.5 ± 197.7	<i>F</i>	1783.8 ± 3388.9	2078.1 ± 3976.9
4 m	2	2210.3 ± 4234.0	2319.0 ± 4439.3	9144.2 ± 202.0	4762.0 ± 4837.7	2263.6 ± 4340.8	<b>1926.3 ± 3666.0</b>
4 m	3	3449.3 ± 3961.3	4670.2 ± 3608.3	9775.1 ± 129.5	5903.4 ± 4194.7	4409.7 ± 5026.2	<b>3402.7 ± 3953.5</b>
4 m	4	<b>2152.1 ± 4126.9</b>	4795.1 ± 5431.6	9617.7 ± 224.8	8055.4 ± 1451.6	4582.6 ± 5204.8	2301.9 ± 4426.5
4 m	5	6969.2 ± 4582.9	<b>5955.7 ± 3973.0</b>	9573.0 ± 229.7	8630.4 ± 2381.1	6913.1 ± 4549.0	6705.8 ± 4456.2
4 m	6	<b>6132.8 ± 842.3</b>	8208.1 ± 1158.6	<i>F</i>	7688.5 ± 623.2	6251.3 ± 2277.5	7990.8 ± 1147.7
<b>Average</b>		<b>4052.1 ± 2135.0</b>	<i>F</i>	<i>F</i>	7070.4 ± 3146.3	<i>F</i>	4335.2 ± 1955.8

Table S2. Loss term ablation. Mean Absolute Error (MAE) of RPM (lower is better) under 4-fold cross-validation on the *Timestamped Quadcopter with Egomotion* (TQE) dataset, reported for two camera–target distances (2 m / 4 m) and seven egomotion levels  $M_{\text{ego}}$ . “All” uses the full batch objective in Eq. (4) with: phase–geometry alignment  $r_\phi$ , radial centering  $r_r$ , polarity alignment  $r_{\text{pol}}$ , soft annulus barriers  $r_{\text{in}}, r_{\text{out}}$ , and Balanced Tip Occupancy  $\ell_{\text{BTO}}$ . Each ablation zeroes the indicated coefficient ( $\lambda_\phi, \lambda_r, \lambda_{\text{pol}}, \lambda_{\text{band}}, \lambda_{\text{BTO}}$ ). TQE ground-truth RPM has  $\mu \pm \sigma = 11193.5 \pm 3540.2$ . Values are mean  $\pm$  std.

modestly. This is consistent with BTO’s role in discouraging degenerate “only-inside/only-outside” fits rather than driving the solution on its own.

Overall, the *phase* and *radial* data terms provide the backbone for stable pose/phase coupling. The *band* constraints and *polarity* alignment significantly boost robustness under distance and high  $M_{\text{ego}}$ ; and *BTO* offers a small but reliable safety margin against occupancy imbalance. Together, these components are necessary to keep the asynchronous EKF and batched GN updates coherent.

$d$	$M_{\text{ego}}$	propeller	MArE (%) ↓			MAE (RPM) ↓			RMSE (RPM) ↓		
			ours	AEB [15]	DeepEv [4]	ours	AEB [15]	DeepEv [4]	ours	AEB [15]	DeepEv [4]
2 m	1	rear right	<b>1.3</b>	61.4	8564.8	<b>93.7</b> ✓	5980.8	652423.7	<b>215.9</b>	7186.8	785896.2
		rear left	1.3	<b>0.9</b>	402.4	81.4 ✓	<b>73.0</b>	32090.3	241.4	<b>241.2</b>	46466.0
		front left	<b>1.5</b>	35.3	4132.0	<b>118.4</b> ✓	2487.0	303141.3	<b>194.1</b>	3302.9	359054.3
		front right	<b>1.2</b>	65.5	94.6	<b>77.8</b> ✓	5650.8	8759.2	<b>186.3</b>	7673.3	9700.4
	2	rear right	<b>1.2</b>	52.1	9523.5	<b>85.0</b> ✓	4637.6	749060.3	<b>178.9</b>	5549.9	904654.7
		rear left	1.3	<b>1.2</b>	4811.7	<b>87.0</b> ✓	112.9	357676.3	<b>277.2</b>	457.4	455119.6
		front left	<b>1.5</b>	49.8	478.5	<b>114.0</b> ✓	3075.8	28118.0	<b>223.5</b>	3879.2	68394.5
		front right	<b>1.1</b>	34.5	7458.3	<b>74.3</b> ✓	2035.8	562988.0	<b>160.9</b>	3367.3	787219.5
	3	rear right	<b>1.2</b>	1198.7	5013.6	<b>85.1</b> ✓	102482.5	386360.6	<b>223.2</b>	192935.8	437954.9
		rear left	31.7	<b>15.0</b>	2059.8	2137.8 ×	<b>1696.4</b>	151319.8	4518.8	<b>3482.9</b>	184206.2
		front left	<b>4.2</b>	467.5	5236.2	<b>230.2</b> ✓	37691.4	376231.1	<b>763.8</b>	81016.3	448776.7
		front right	<b>4.8</b>	1347.9	195.7	<b>267.9</b> ✓	110056.2	14595.8	<b>1031.9</b>	202948.8	18910.5
4 m	4	rear right	<b>80.2</b>	1241.2	12474.4	<b>7634.3</b> ×	93995.4	934583.8	<b>9184.5</b>	182884.8	1141131.4
		rear left	72.2	<b>24.5</b>	8678.3	7135.2 ×	<b>2828.9</b>	674615.2	8699.8	<b>4782.1</b>	824811.5
		front left	<b>79.3</b>	410.3	89.2	<b>7249.8</b> ×	29227.1	8417.0	<b>8825.0</b>	68684.3	9362.8
		front right	76.3	<b>59.5</b>	115.2	6830.5 ×	<b>5933.1</b>	9027.6	<b>8459.0</b>	11580.7	10408.5
	5	rear right	<b>62.3</b>	531.3	106.7	<b>6347.2</b> ×	41415.3	9244.0	<b>7842.7</b>	79321.0	10241.1
		rear left	<b>100.9</b>	480.0	117.9	<b>9689.7</b> ×	30491.9	10624.2	<b>10899.5</b>	67097.7	12239.0
		front left	<b>65.0</b>	389.8	99.3	<b>5045.3</b> ×	33458.3	8963.0	<b>6266.7</b>	69659.2	9836.3
		front right	<b>97.7</b>	1122.0	398.5	<b>8871.4</b> ×	77151.0	32523.2	<b>9710.6</b>	111267.4	56823.0
	6	rear right	<b>93.6</b>	726.2	98.1	<b>8928.2</b> ×	56816.8	9461.9	<b>9874.9</b>	72370.2	10223.4
		rear left	<b>97.2</b>	593.1	108.1	<b>9221.9</b> ×	41752.5	9932.7	<b>10100.1</b>	56316.4	11232.3
		front left	<b>89.5</b>	885.2	103.3	<b>8283.4</b> ×	61735.0	9163.9	<b>9331.8</b>	72061.8	10279.6
		front right	<b>57.2</b>	833.4	96.8	<b>5492.3</b> ×	58682.1	8881.7	<b>6655.9</b>	72261.9	9697.5
7	rear right	<b>72.2</b>	609.8	10417.8	<b>7194.7</b> ×	44713.1	780191.6	<b>8292.1</b>	51904.1	894151.1	
	rear left	119.1	617.6	<b>97.0</b>	<b>8328.7</b> ×	45454.3	9180.8	10071.3	51421.3	<b>10022.4</b>	
	front left	<b>75.7</b>	218.3	96.4	<b>5341.7</b> ×	16859.6	8811.8	<b>6817.1</b>	28904.6	9686.0	
	front right	<b>72.2</b>	248.4	3638.0	<b>5124.5</b> ×	17502.1	253240.6	<b>6262.9</b>	29616.6	315329.1	
4 m	1	rear right	<b>73.1</b>	285.5	834.5	<b>6616.3</b> ×	21029.7	57801.3	<b>8517.8</b>	46759.1	73901.3
		rear left	<b>1.2</b>	57.2	89.6	<b>76.4</b> ✓	6038.7	8341.9	<b>158.4</b>	20115.0	9422.8
		front left	<b>1.4</b>	48.9	88.7	<b>104.8</b> ✓	4676.4	7853.7	<b>255.3</b>	16769.4	8925.9
		front right	<b>1.3</b>	165.4	835.4	<b>87.8</b> ✓	13041.8	58054.3	<b>319.4</b>	36853.1	74833.5
	2	rear right	91.1	<b>43.1</b>	93.1	8561.2 ×	<b>3847.8</b>	8671.9	9537.1	<b>4496.9</b>	9642.0
		rear left	<b>1.3</b>	37.4	3242.1	<b>85.7</b> ✓	3529.9	241975.2	<b>273.2</b>	5020.2	334534.1
		front left	<b>1.5</b>	72.1	93.8	<b>112.9</b> ✓	6545.9	8536.3	<b>254.1</b>	17753.2	9595.1
		front right	<b>1.3</b>	77.3	111.7	<b>81.4</b> ✓	4335.3	8969.8	<b>248.9</b>	17551.4	10429.0
	3	rear right	70.9	<b>58.8</b>	95.8	<b>5770.0</b> ×	5904.9	9773.3	<b>7008.1</b>	11479.0	10725.7
		rear left	<b>1.3</b>	46.8	1801.4	<b>85.0</b> ✓	3960.0	140787.4	<b>211.7</b>	4845.4	181653.8
		front left	<b>1.3</b>	303.1	1937.2	<b>109.4</b> ✓	21349.0	146814.9	<b>210.8</b>	51357.9	174482.0
		front right	79.8	<b>39.7</b>	97.4	7832.8 ×	<b>4091.3</b>	9594.5	9394.6	<b>5306.3</b>	10465.4
4	rear right	<b>83.5</b>	1194.9	95.2	<b>8342.3</b> ×	101987.0	9517.6	<b>9491.6</b>	201102.2	10384.6	
	rear left	<b>1.1</b>	915.1	5251.8	<b>77.6</b> ✓	76275.0	426131.2	<b>222.5</b>	179370.3	537350.6	
	front left	<b>1.4</b>	1392.2	389.6	<b>111.6</b> ✓	98307.7	26933.9	<b>288.4</b>	201185.3	46853.8	
	front right	<b>1.2</b>	1166.3	13.3	<b>76.9</b> ✓	86077.0	693.4	<b>209.4</b>	191384.9	2370.2	
5	rear right	<b>95.3</b>	994.6	97.8	<b>9688.6</b> ×	83816.5	9942.3	<b>10614.2</b>	127547.1	10817.5	
	rear left	<b>93.9</b>	1043.3	94.8	<b>9316.3</b> ×	76882.9	9332.0	10400.6	133235.2	<b>10351.1</b>	
	front left	<b>1.7</b>	1092.8	3339.1	<b>119.1</b> ✓	81598.8	260136.5	<b>241.1</b>	126119.1	310936.4	
	front right	<b>88.3</b>	1126.9	95.6	<b>8752.7</b> ×	93336.6	9351.7	<b>9711.9</b>	134050.9	10281.2	
6	rear right	<b>62.1</b>	862.2	167.5	<b>6778.5</b> ×	68419.4	14322.1	<b>8015.9</b>	97991.7	20098.2	
	rear left	<b>57.6</b>	958.9	3772.0	<b>5547.2</b> ×	71680.8	290173.7	<b>6746.4</b>	101283.8	359570.3	
	front left	<b>71.5</b>	995.9	11718.5	<b>6929.4</b> ×	76394.7	918479.2	<b>8522.6</b>	105034.9	1024071.7	
	front right	<b>60.3</b>	856.0	130.4	<b>5276.0</b> ×	68594.4	12657.2	<b>6397.8</b>	102062.7	18155.9	

Table S3. Benchmark, Timestamped Quadcopter with Egomotion (TQE). For each presented method and setting (camera-target distance  $d$ , egomotion level  $M_{\text{ego}}$ ), the average shaft-RPM mean absolute relative error (MArE), mean absolute error (MAE), and root mean squared error (RMSE) are reported over 4-fold cross-validation across the four propellers (one training propeller per fold). Both AEB-Tracker [15] and DeepEv [4] methods were modified to allow RPM estimation (see Sec. 4.3). TQE ground-truth RPM has  $\mu \pm \sigma = 11193 \pm 3540$ , min 917, max 15768.  $M_{\text{ego}} = 1$  roughly means “slow camera movement”, while  $M_{\text{ego}} = 5$  means “fast camera movement” (see Fig. 2). As  $M_{\text{ego}}$  increases, the camera experiences stronger egomotion, leading to increase of the number of events generated in the background.

$rb$	$\Delta t$	$q_{xy}$	$q_q$	MArE (%)	↓	median	MAE (RPM)	↓	median
22	2	0.2	0.25	496.419 ± 402.402		428.662	39026.775 ± 35704.452		27149.123
22	2	0.2	0.5	538.978 ± 532.238		335.813	41383.706 ± 40575.234		24252.682
22	2	0.2	1	650.760 ± 610.255		580.914	49669.433 ± 45197.183		44281.303
22	2	0.2	2	697.412 ± 668.144		537.904	53110.765 ± 50873.870		39796.295
22	2	1	0.25	587.555 ± 478.454		411.100	39086.051 ± 29527.280		26570.284
22	2	1	0.5	544.618 ± 510.582		401.498	41860.949 ± 39341.854		30303.074
22	2	1	1	615.645 ± 577.918		553.496	47675.376 ± 44307.127		42378.293
22	2	1	2	694.885 ± 662.955		577.022	52290.860 ± 49815.795		42225.829
22	2	5	0.25	510.618 ± 388.804		397.497	39608.748 ± 29903.648		29931.931
22	2	5	0.5	506.789 ± 472.468		400.054	38952.001 ± 36484.847		29859.506
22	2	5	1	637.420 ± 590.571		597.896	48856.215 ± 44965.901		44515.639
22	2	5	2	664.801 ± 623.023		618.496	50721.102 ± 47445.002		46145.155
22	2.5	0.2	0.25	599.204 ± 405.217		428.662	39154.585 ± 31844.812		27149.123
22	2.5	0.2	0.5	541.204 ± 535.575		335.813	41498.917 ± 40751.855		24252.682
22	2.5	0.2	1	656.356 ± 608.960		626.036	50086.419 ± 45131.954		46723.292
22	2.5	0.2	2	700.457 ± 672.777		537.904	53245.557 ± 51105.783		39796.295
22	2.5	1	0.25	582.944 ± 578.059		404.861	39748.436 ± 29535.466		26218.892
22	2.5	1	0.5	546.194 ± 513.463		401.498	41776.215 ± 39284.539		30303.074
22	2.5	1	1	619.680 ± 584.761		553.496	48030.629 ± 44997.063		42378.293
22	2.5	1	2	696.192 ± 666.004		577.022	52501.734 ± 50255.610		42225.829
22	2.5	5	0.25	511.004 ± 391.626		362.751	39689.789 ± 30294.397		29321.017
<b>22</b>	<b>2.5</b>	<b>5</b>	<b>0.5</b>	<b>502.976 ± 462.531</b>		<b>400.054</b>	<b>38763.807 ± 35860.448</b>		<b>29859.506</b>
22	2.5	5	1	635.099 ± 588.028		597.896	48705.017 ± 44782.988		44515.639
22	2.5	5	2	667.087 ± 627.251		618.496	50801.457 ± 47640.824		46145.155
22	3	0.2	0.25	537.926 ± 339.939		388.690	40797.556 ± 25179.970		32766.673
22	3	0.2	0.5	527.948 ± 330.960		482.435	39522.724 ± 23976.905		36248.414
22	3	0.2	1	1572.458 ± 1439.686		1071.014	118593.768 ± 108749.883		77281.079
22	3	0.2	2	1729.390 ± 1080.637		1360.253	130145.474 ± 80259.290		110851.655
22	3	1	0.25	510.972 ± 337.896		387.988	39089.727 ± 25213.444		29948.624
22	3	1	0.5	522.499 ± 311.308		439.585	39133.979 ± 22301.822		32878.498
22	3	1	1	1623.040 ± 1543.883		999.876	122206.230 ± 115777.126		76014.113
22	3	1	2	1819.391 ± 1076.640		1690.690	137646.186 ± 80980.053		131528.893
22	3	5	0.25	528.778 ± 327.504		393.982	39501.077 ± 24184.137		30356.179
22	3	5	0.5	620.653 ± 478.684		477.139	46596.672 ± 35946.071		36226.416
22	3	5	1	1775.582 ± 1666.385		1223.899	133680.214 ± 125213.233		87960.026
22	3	5	2	1868.451 ± 1043.308		1612.597	140173.319 ± 78815.962		128391.421
33	2	0.2	0.25	532.076 ± 542.658		313.137	40817.897 ± 42290.509		23969.480
33	2	0.2	0.5	637.817 ± 621.567		359.301	49911.826 ± 48999.356		28496.135
33	2	0.2	1	722.345 ± 689.412		658.855	54920.949 ± 53254.591		47154.050
33	2	0.2	2	801.631 ± 764.621		785.360	61030.529 ± 59447.827		53700.933
33	2	1	0.25	539.595 ± 519.382		358.879	41270.586 ± 40010.637		28240.227
33	2	1	0.5	628.204 ± 611.694		431.265	48692.147 ± 47599.814		29409.219
33	2	1	1	756.455 ± 724.681		638.275	57933.012 ± 56141.403		47235.750
33	2	1	2	764.616 ± 729.480		607.390	58027.384 ± 56269.086		46369.599
33	2	5	0.25	594.884 ± 547.826		405.281	45212.128 ± 41849.225		29930.397
33	2	5	0.5	610.897 ± 618.423		408.550	47681.510 ± 48051.032		30428.694
33	2	5	1	767.419 ± 722.414		736.989	58523.058 ± 55635.939		54296.780
33	2	5	2	730.990 ± 714.165		662.121	55352.472 ± 55168.873		49709.951
33	2.5	0.2	0.25	543.074 ± 522.441		313.137	41890.431 ± 41373.974		24346.624
33	2.5	0.2	0.5	639.535 ± 619.235		401.370	50020.820 ± 48816.418		30022.854
33	2.5	0.2	1	727.481 ± 698.813		668.252	55288.661 ± 54127.417		47256.535
33	2.5	0.2	2	796.948 ± 755.814		785.360	60555.252 ± 58419.579		53700.933
33	2.5	1	0.25	532.410 ± 506.342		358.879	41036.682 ± 39777.801		28240.227
33	2.5	1	0.5	628.658 ± 612.606		431.265	48665.147 ± 47531.149		29409.219
33	2.5	1	1	743.469 ± 715.875		624.827	57122.147 ± 55425.865		45484.744
33	2.5	1	2	768.513 ± 746.872		601.761	58471.489 ± 57907.022		45485.936
33	2.5	5	0.25	580.653 ± 485.517		490.506	44371.759 ± 38134.757		35223.893
33	2.5	5	0.5	611.000 ± 617.790		408.550	47776.018 ± 48238.017		30428.694
33	2.5	5	1	760.575 ± 742.399		681.596	58266.260 ± 57509.586		48980.242
33	2.5	5	2	727.158 ± 722.614		597.588	54981.420 ± 55610.817		46677.389
33	3	0.2	0.25	780.803 ± 691.614		539.572	56835.266 ± 50675.677		40003.480
33	3	0.2	0.5	711.595 ± 534.618		538.977	52049.844 ± 39029.338		41273.869
33	3	0.2	1	1334.438 ± 1139.468		903.428	98922.204 ± 83349.423		68183.272
33	3	0.2	2	1800.403 ± 1083.555		1388.857	133261.705 ± 80987.728		101892.368
33	3	1	0.25	797.649 ± 670.641		528.780	58814.987 ± 49205.799		37539.753
33	3	1	0.5	752.721 ± 578.674		586.153	56295.285 ± 43346.004		42539.879
33	3	1	1	1371.708 ± 1131.488		885.898	100812.434 ± 83139.604		65690.880
33	3	1	2	1882.050 ± 1109.445		1727.309	138601.952 ± 83147.089		128224.109
33	3	5	0.25	705.389 ± 592.629		559.554	52950.606 ± 43547.516		42432.900
33	3	5	0.5	713.524 ± 573.891		534.925	52982.647 ± 42424.617		39459.804
33	3	5	1	1401.862 ± 1125.218		929.897	102499.465 ± 82047.435		64251.491
33	3	5	2	1843.070 ± 1090.486		1565.962	136415.532 ± 80887.240		122453.756

Table S4. AEB-Tracker grid search results. MAE and MArE reported as  $\mu \pm \sigma$ . See Sec. S4 for description.